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The risk and reliability of hydrogen as a sustainable energy source

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Outlines

- ✓ Introduction
- ✓ Risk and Reliability in Engineering Operations
- ✓ Hydrogen safety
- ✓ Cases studied

 Photovoltaics and Solar Energy	 Hydrogen		 Grid integration	 Energy Economics
Director, Shujuan Huang	Director, Fatemeh Salehi		Director, Sara Deilami	Director, Stefan Trueck
<ul style="list-style-type: none">• development of photovoltaic materials for next generation high efficiency solar cells• development of device fabrication technologies to reduce the cost of power generation	<p><i>Production and Utilisation</i></p> <ul style="list-style-type: none">• bio-hydrogen production to increase the rate and yield of hydrogen production with minimal by-products• Chemical production of hydrogen using a sustainable chemical looping process	<p><i>Application and Safety</i></p> <ul style="list-style-type: none">• provide scientific and technical knowledge in understanding the safety aspects related to hydrogen energy applications• risk analysis and consequence modelling regarding hydrogen applications	<ul style="list-style-type: none">• energy management and distribution for commercial and residential systems, micro grid and grid integration• integration of electrical vehicles into the grid for charging and supply	<ul style="list-style-type: none">• Financial innovation strategies to stabilise energy markets transitioning from fossil-fuel fired power generation to a renewable energy model

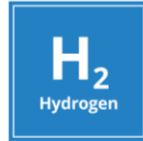
Introduction



Green
Hydrogen
(Decarbonized)



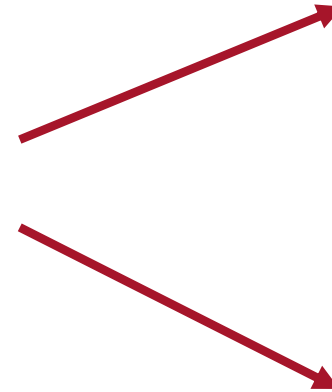
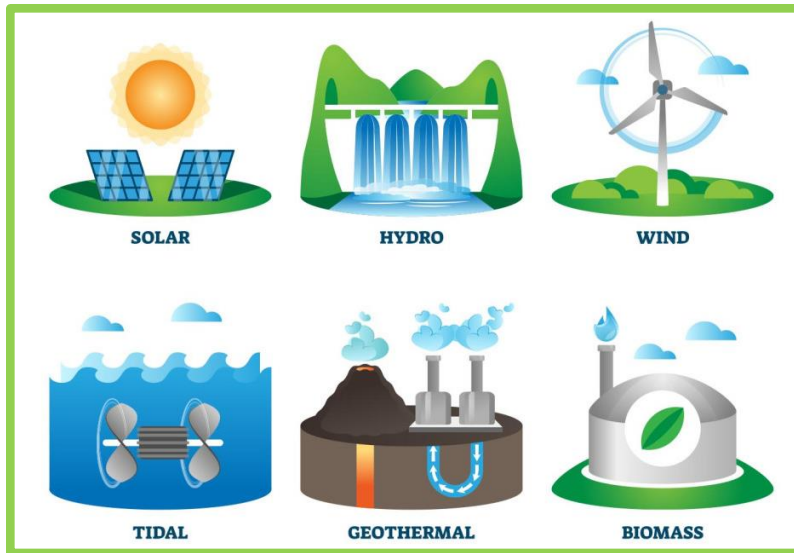
Grey
Hydrogen



Blue
Hydrogen
(Decarbonized)



Brown
Hydrogen



Hydrogen characteristics

- High energy density
- Storage options
- Environmentally friendly
- Non-toxic
- Availability

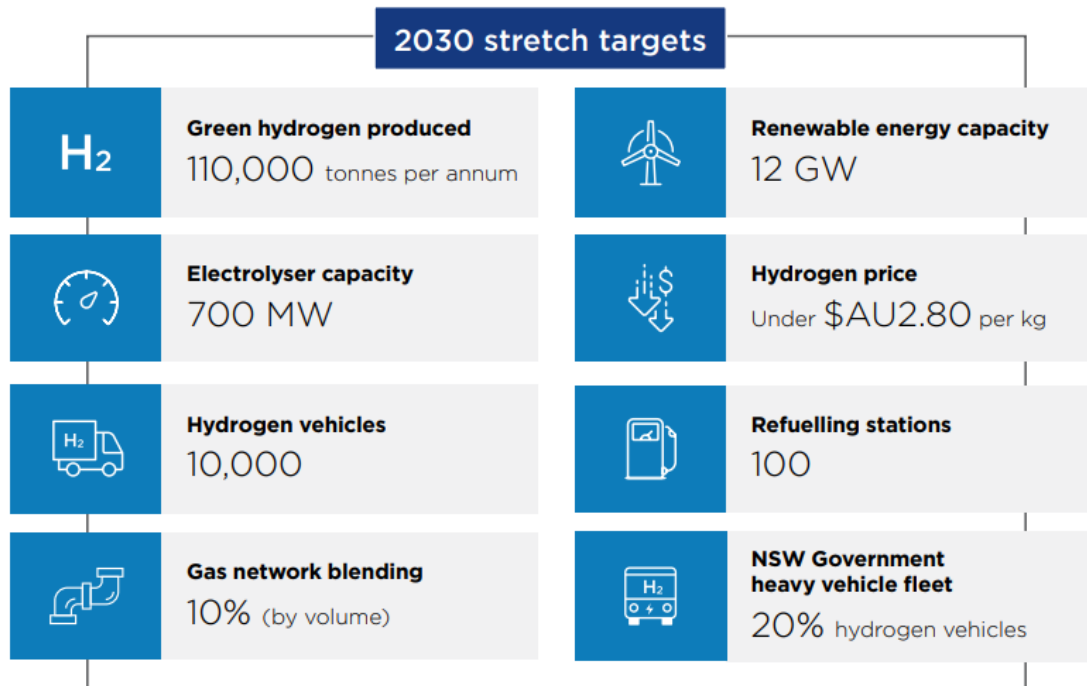
Introduction

International Partnership for Hydrogen and Fuel Cells in the Economy



Introduction

- The Council of Australian Governments (COAG) Energy Council
- National Hydrogen Strategy Taskforce



Risk Assessment

Risk

Assessment of the presence and impact of unwanted situation at time t

Risk (t) = occurrence of unwanted situations & its impact

$$Risk(t) = F(t) \cdot Loss(t)$$

Safety

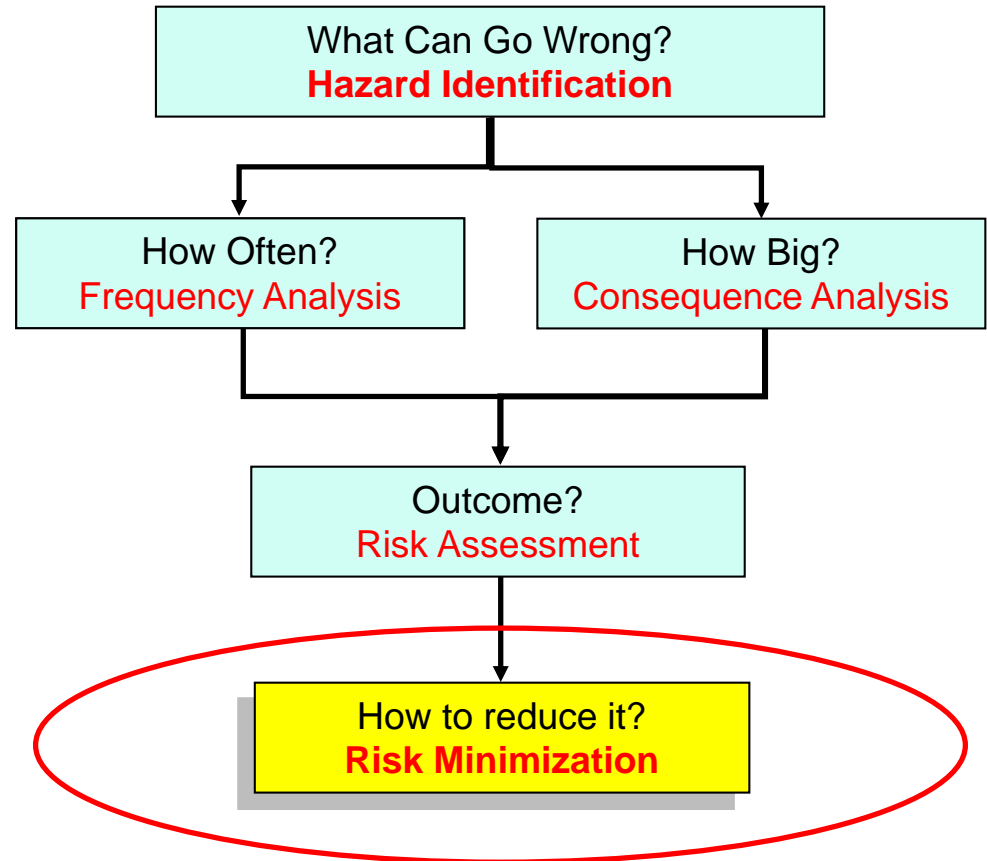
Absence of unwanted situation in system/operation at time t

$$S(t) \propto \frac{1}{Risk(t)}$$

Reduce Risk

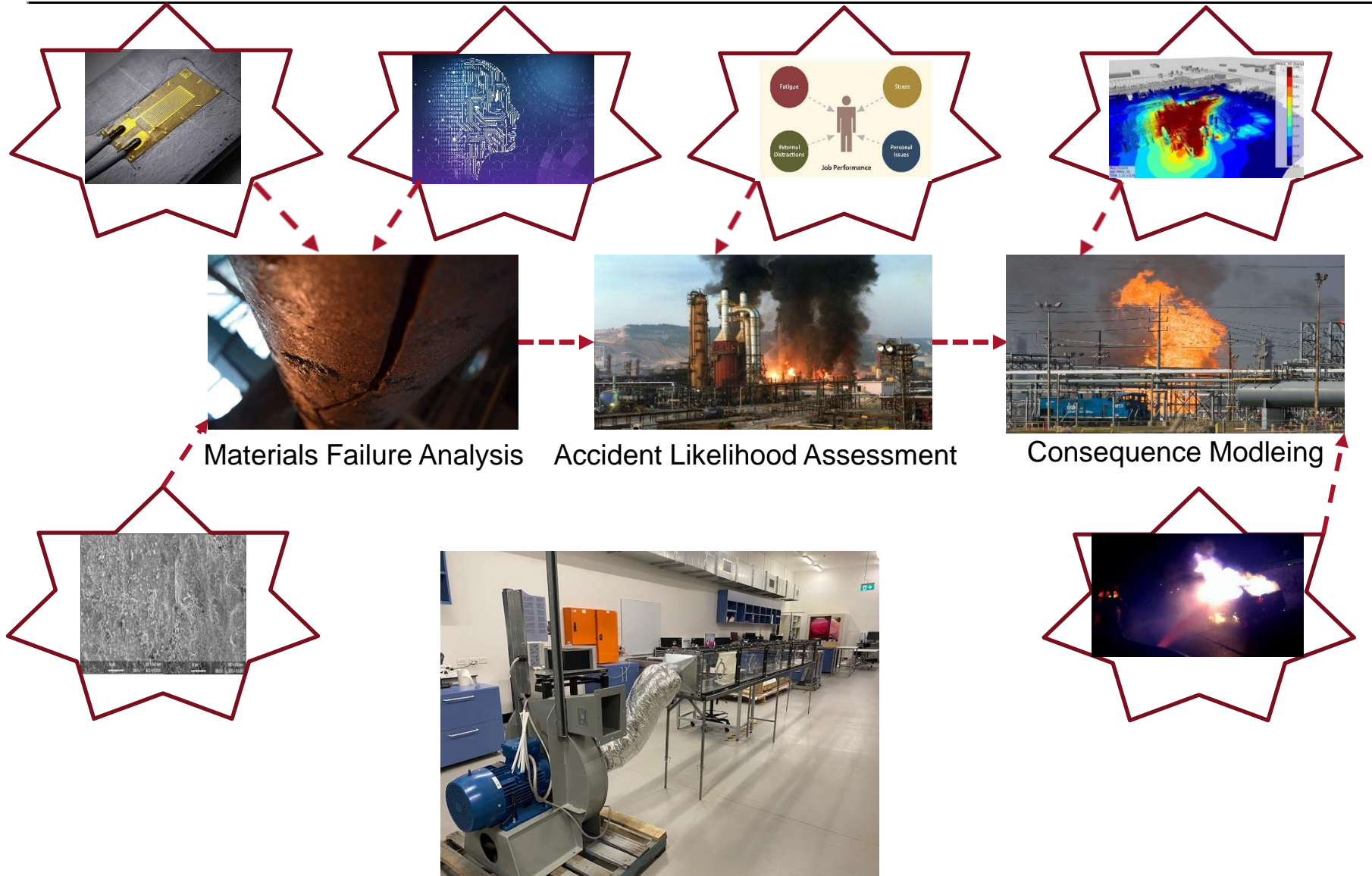
Reduce likelihood (probability)

Reduce impact



Scope of Our Research

Risk, Safety and Reliability Engineering



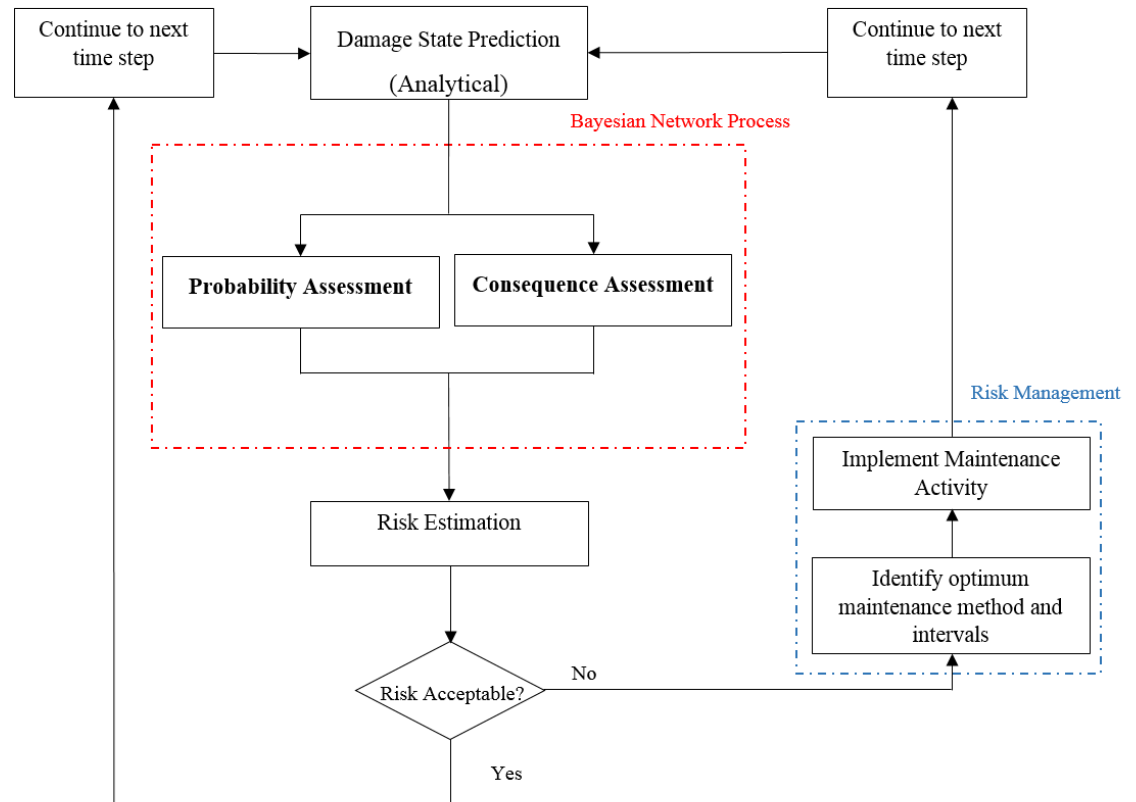
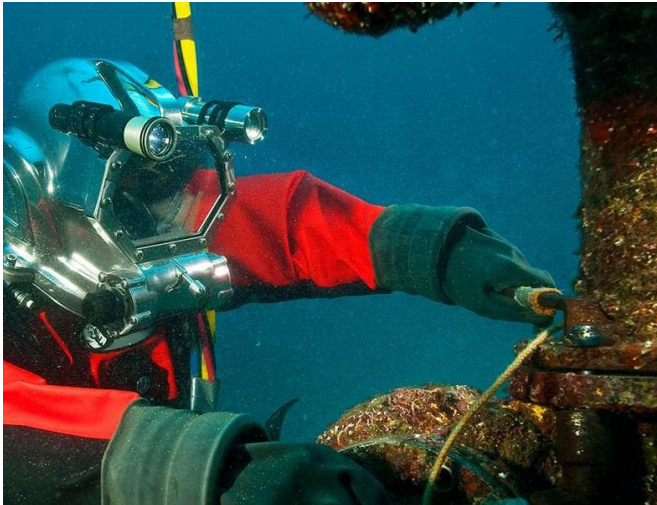
Inspection & Maintenance Planning



Optimization of **repair/service schedule** with an aim to **minimize cost** and **maximize safety & availability**



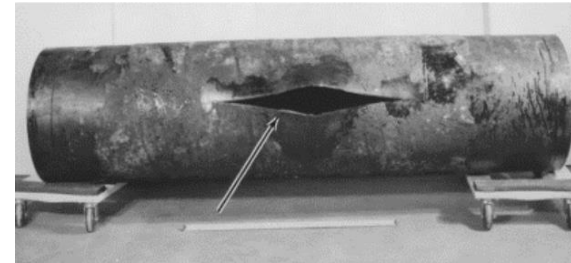
Risk-Based Maintenance



Dynamic Fatigue Crack Modeling

$$\frac{da}{dN} = C(\Delta K)^m \quad \text{Paris' law for fatigue damage}$$

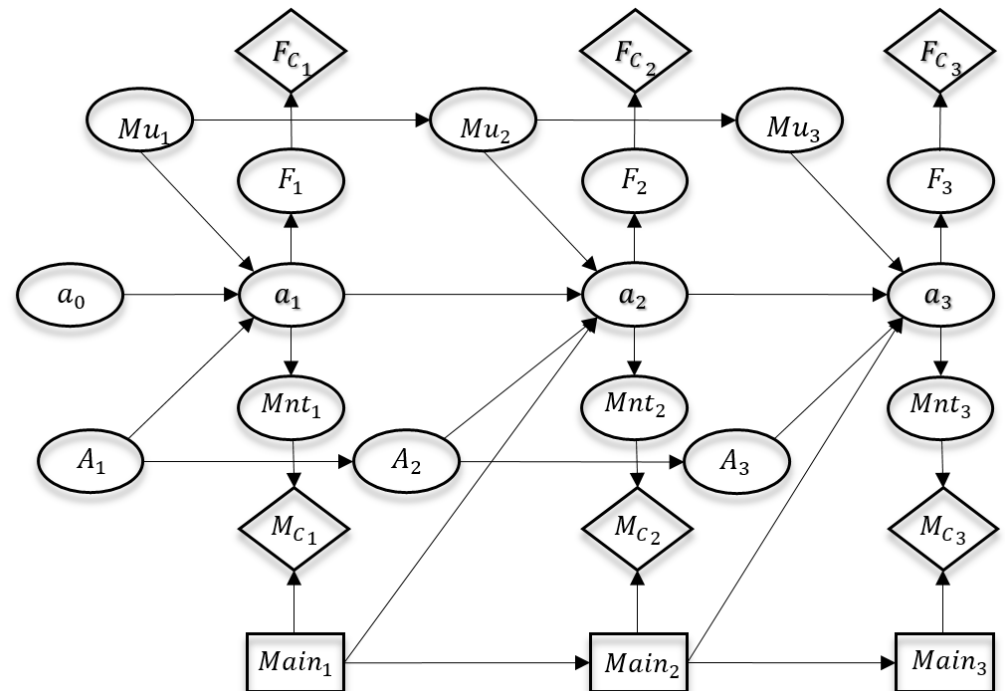
$$a_i = \left(a_{i-1}^{\frac{2-m}{2}} + M_U K A^m \right)^{\frac{2}{2-m}}, m \neq 2$$



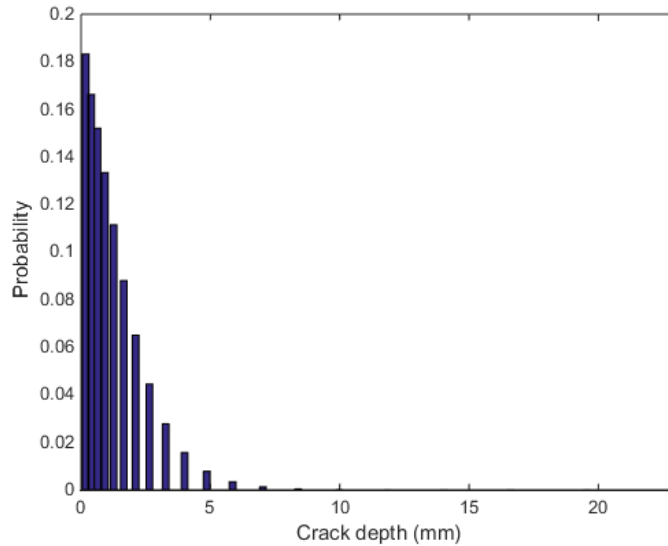
Limit State

$$F_i = a_c - a_i \quad \begin{cases} F_i > 0 & \text{safe} \\ F_i \leq 0 & \text{fail} \end{cases}$$

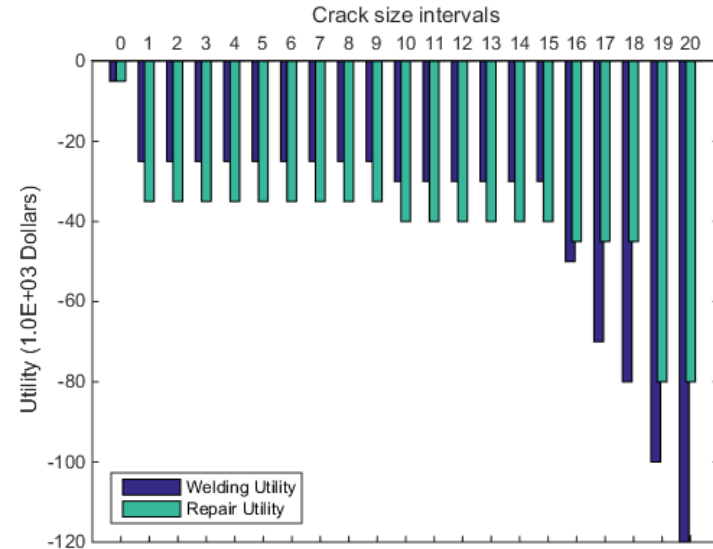
Variable	Description
a_0	Initial crack depth
a_i	Actual crack depth
N	Load cycles
ΔK	Stress intensity factor
C, m	Material parameters
F_i	Failure Function
A	Weibull scale parameter
M_U	Model uncertainty
Mnt	Crack detection
M_c	Maintenance cost
F_c	Failure cost



Crack Size and Cost



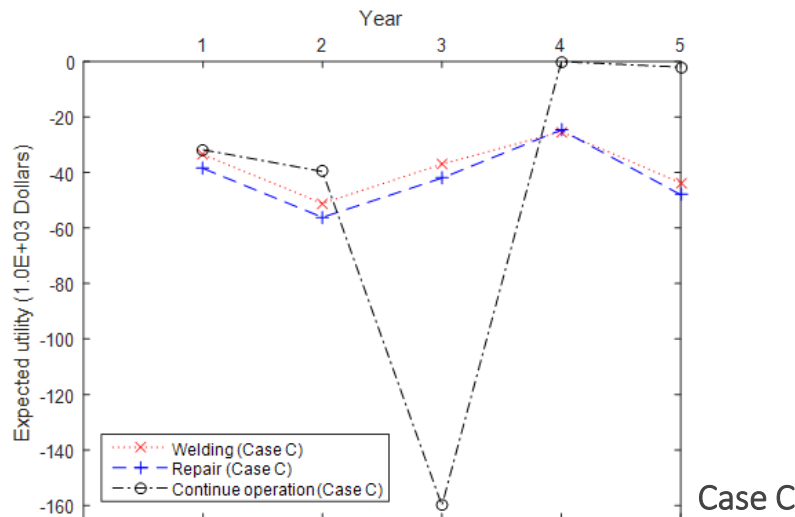
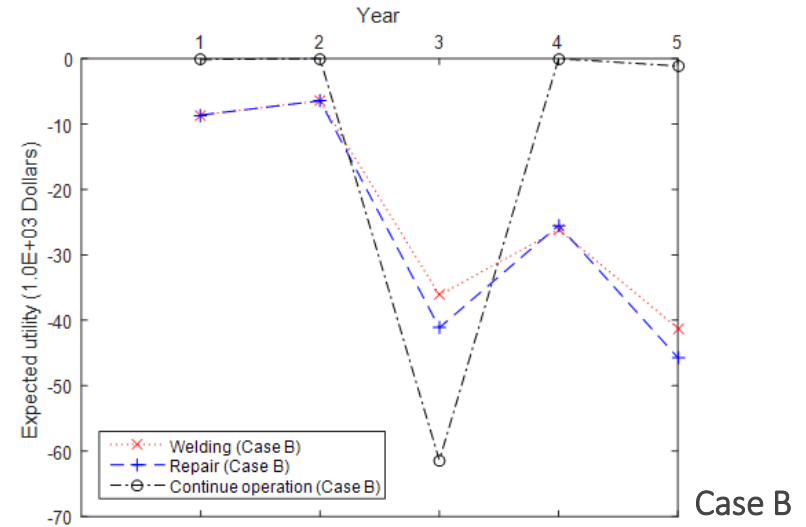
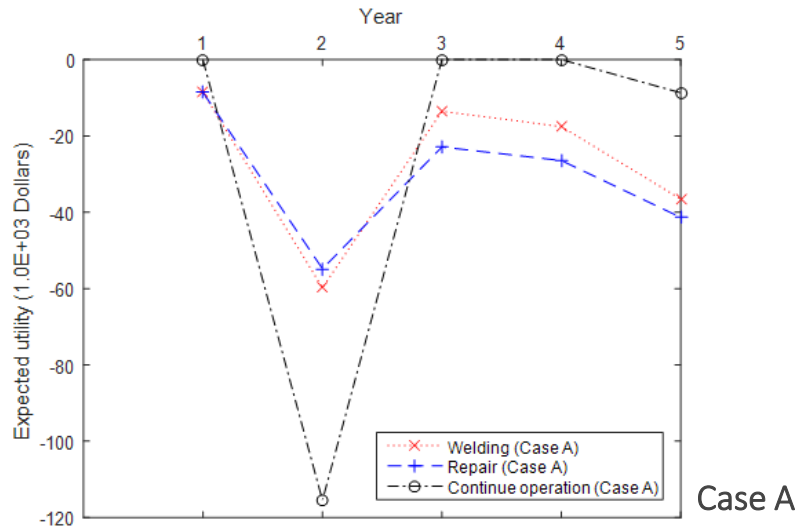
Initial crack size distribution (a_0)



Utility functions of decision alternatives

Year	1	2	3	4	5
Case A	No Detection	State 15	-	-	-
Case B	No Detection	No Detection	State 11	-	-
Case C	State 8	State 12	State 14	-	-

Comparison Results



Year	1	2	3	4	5
Case A	No Det.	State 15	-	-	-
Case B	No Det.	No Det.	State 11	-	-
Case C	State 8	State 12	State 14	-	-

Hydrogen accidents

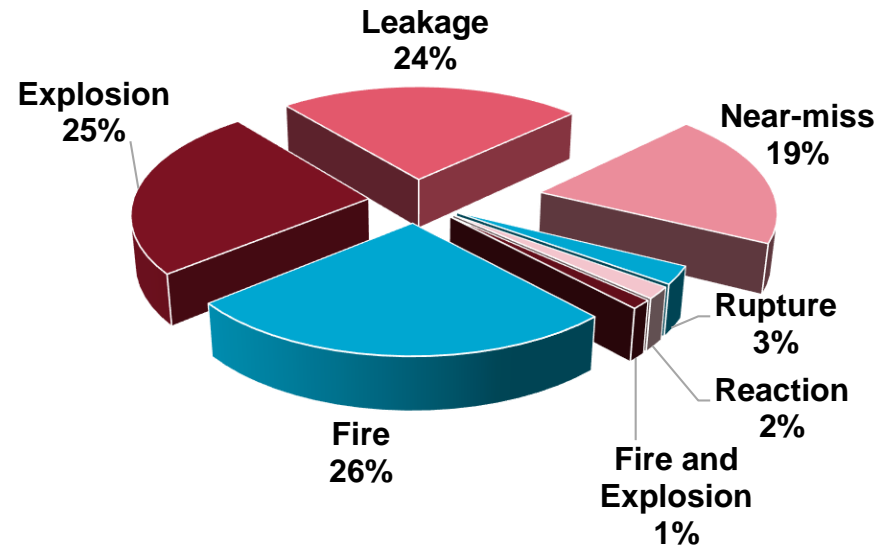
230 accidents over the last two decades: (H2Tool database)

Major causes

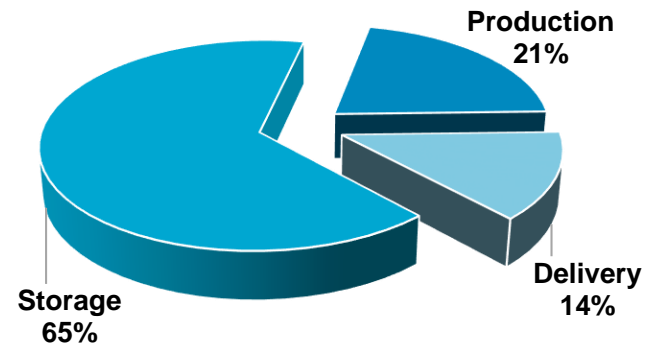
- Human errors
- Equipment failures
- Design issues

Consequences

- Property damage
- Injury to human
- Loss of human life

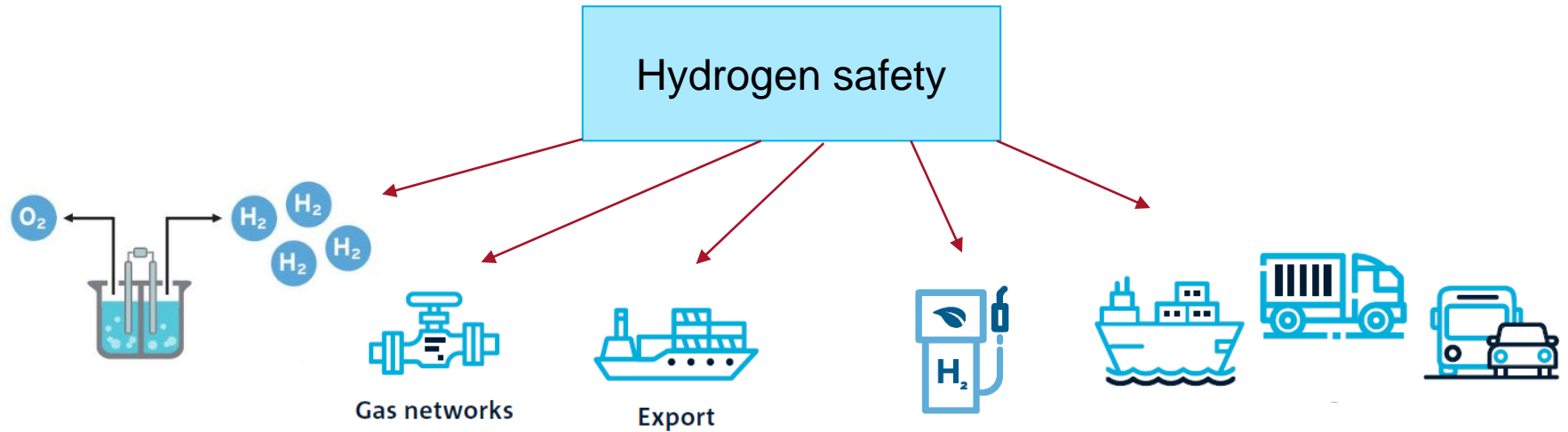


Accident



Facility

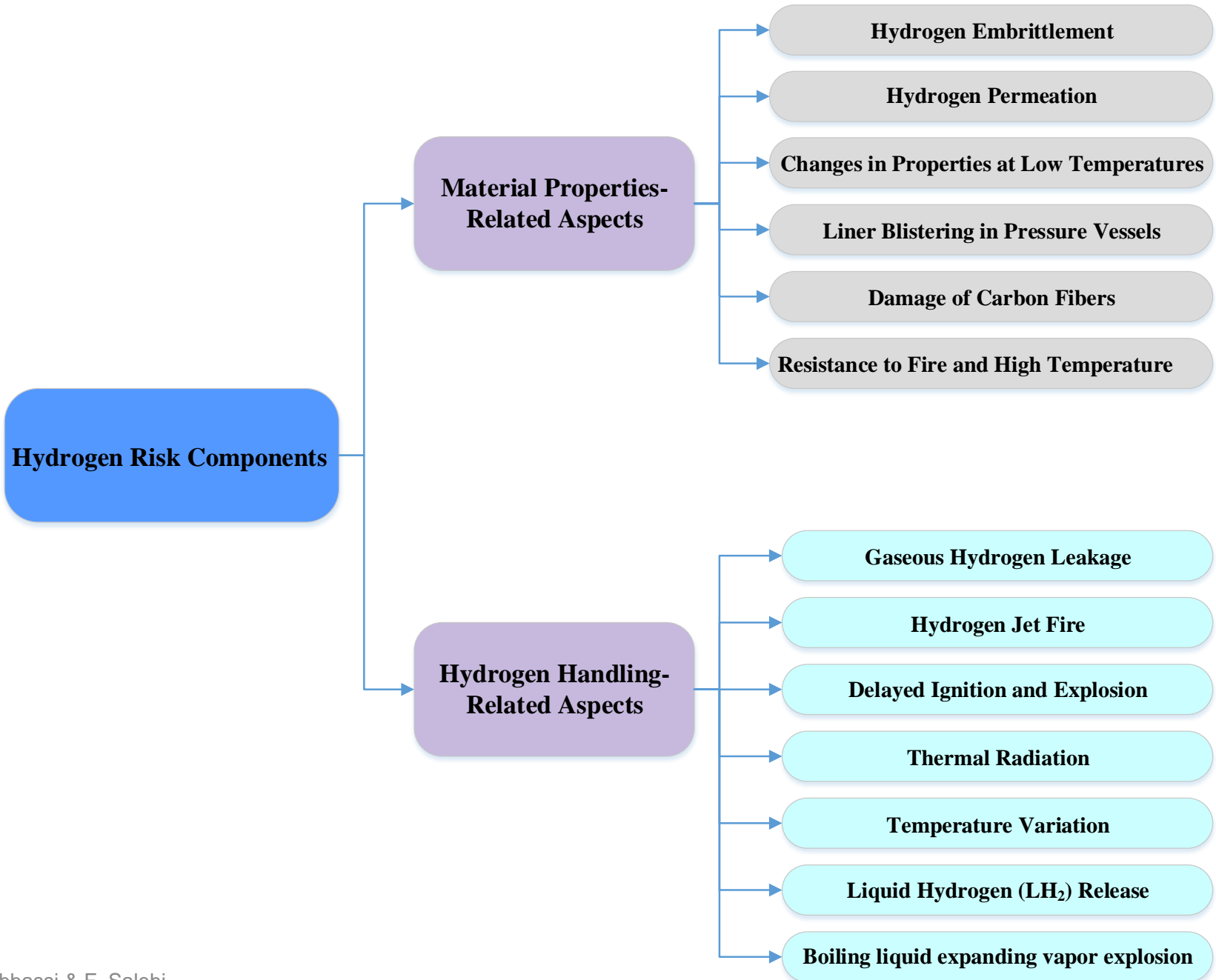
Hydrogen safety



Liquid Hydrogen



Gaseous Hydrogen



Hydrogen Safety: Challenges with Current Modeling

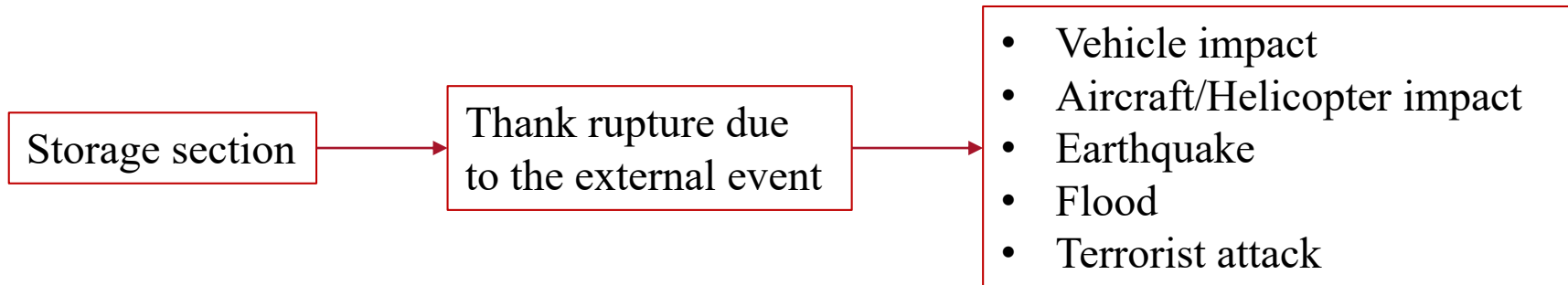
- ✓ Safety of hydrogen infrastructures are vital in the growth of hydrogen economy
- ✓ Several risk models have been developed to assess the safety of hydrogen infrastructures, however, most of them have the shortcomings of:
 - Being static in nature, not properly observing the variability occurring in operation via time
 - Lack of enough precise data of young emerging technologies like hydrogen which leads to uncertainty in input and output parameters
 - Lack of considering the dependencies among the root failures of complex systems
 - Attending to mechanical failures without paying enough attention to human and organizational failures

Failures considered in:

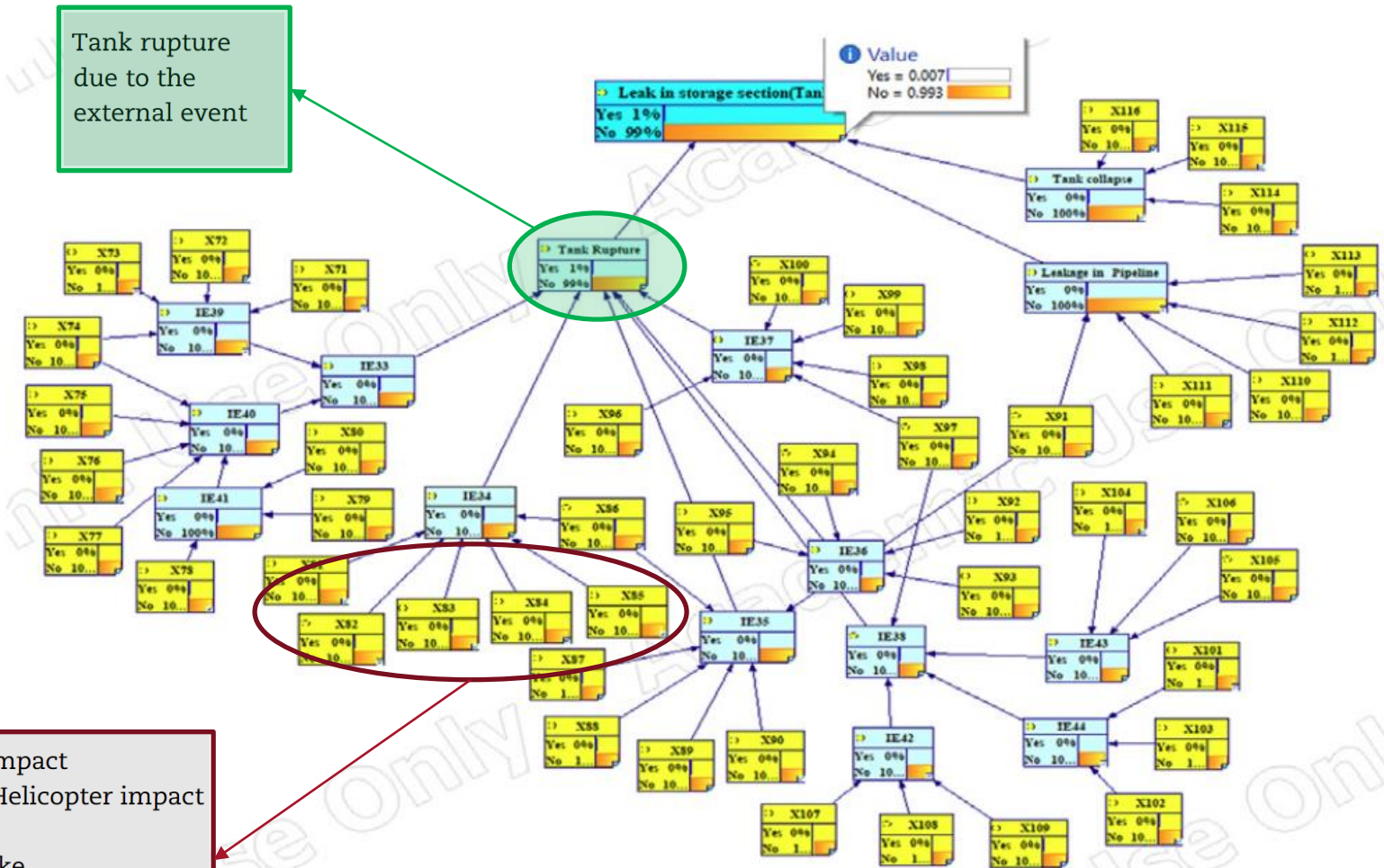
- Chemical section
- Mechanical section
- Storage section

Cause-effect model of the hydrogen release accident scenario

- Failure and causes:
 - ✓ Identify all possible failures of the main equipment, leading to a hydrogen leak,
 - ✓ How failures are connected and how they can logically lead to the accident scenario
- Likelihood values for each cause
 - Background history
 - Expert judgment (use conventional methods)



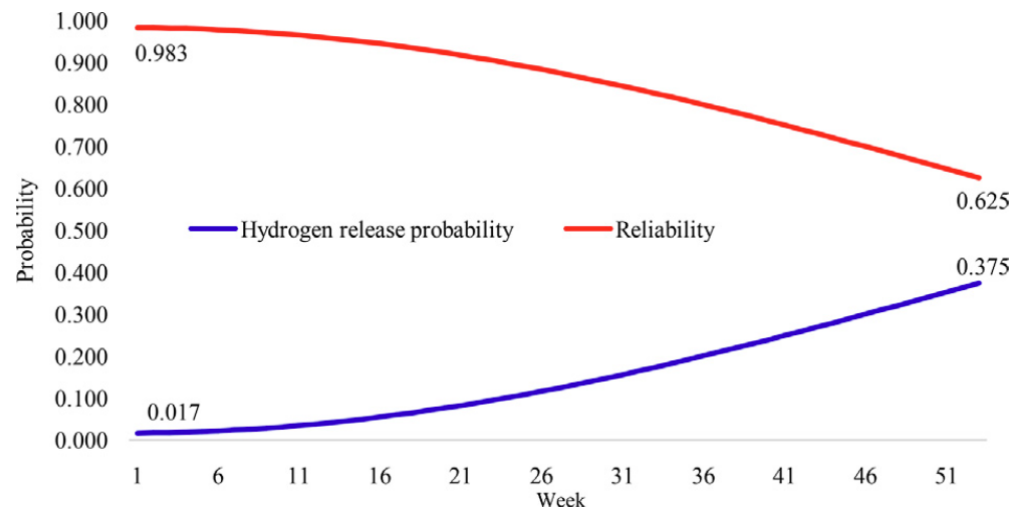
Hydrogen safety – production site



- X81 Vehicle impact
- X82 Aircraft/Helicopter impact
- X83 Earthquake
- X84 Heavy storms
- X85 Flood
- X86 Terrorist attack

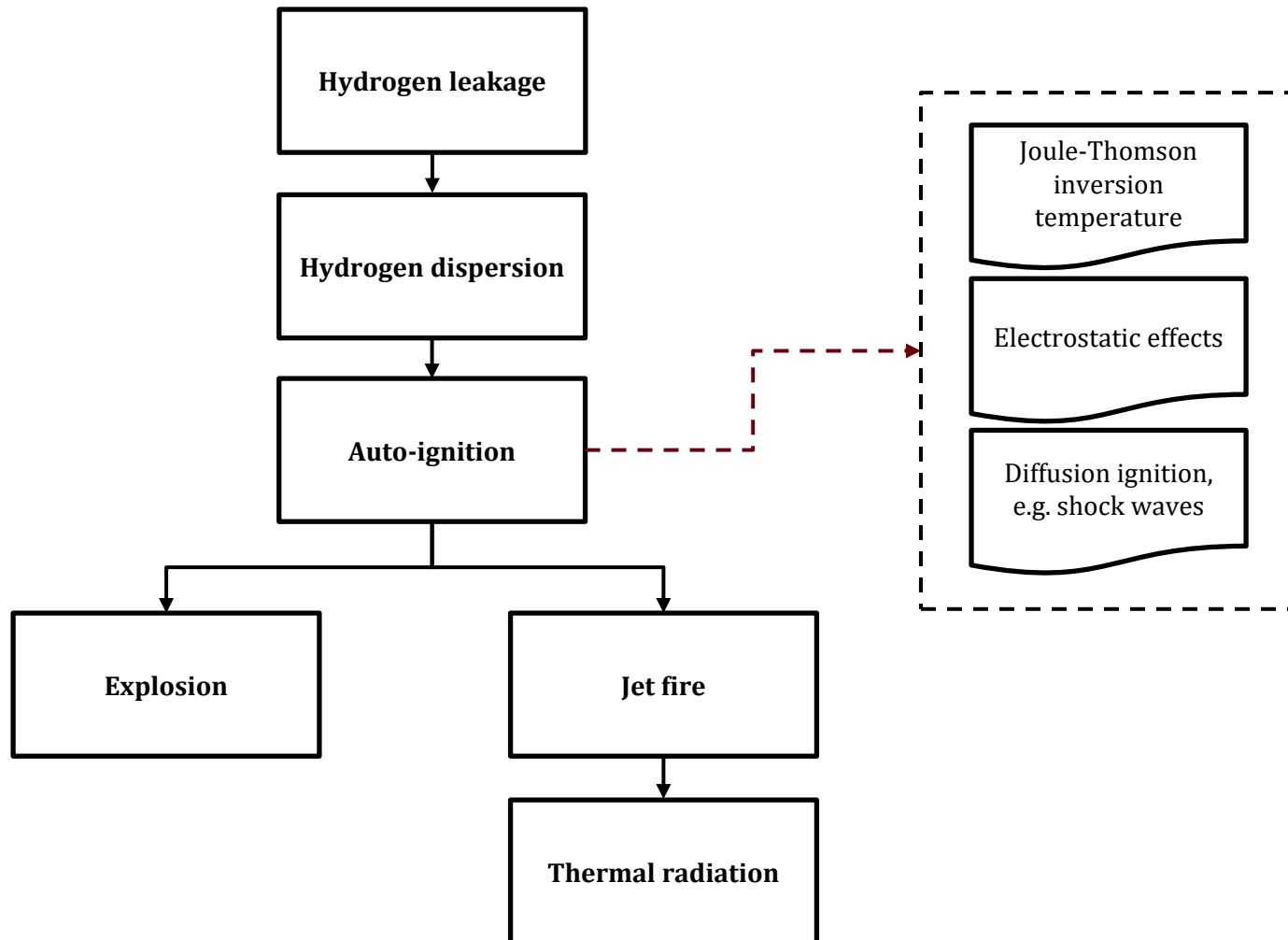
Hydrogen safety - Production site

- ✓ A significant change in the system reliability within a year confirms the system degrades dramatically during the considered time interval



- ✓ Dynamic modelling of hydrogen release probability and the system reliability
 - Safety barriers
 - Backward analysis: find critical cause of accident

Hydrogen Accidents: Consequence Modelling



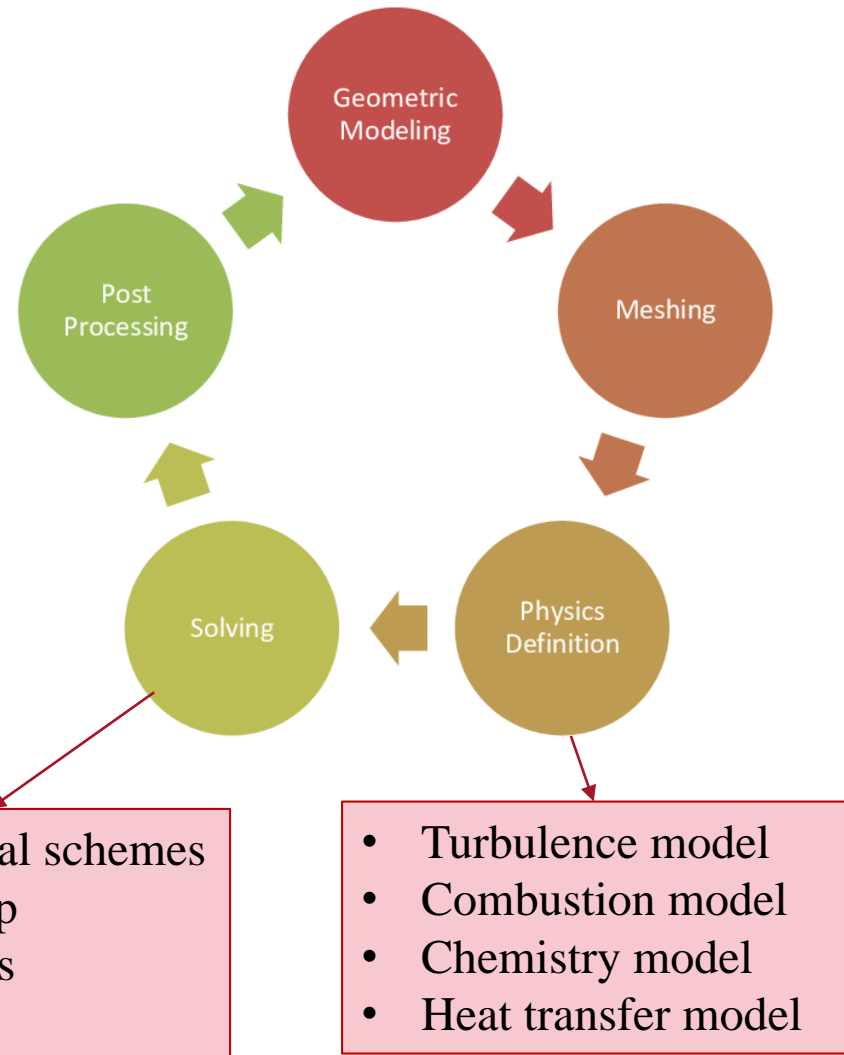
Governing equations

$$\frac{\partial \bar{\rho}}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_i}{\partial x_i} = 0$$

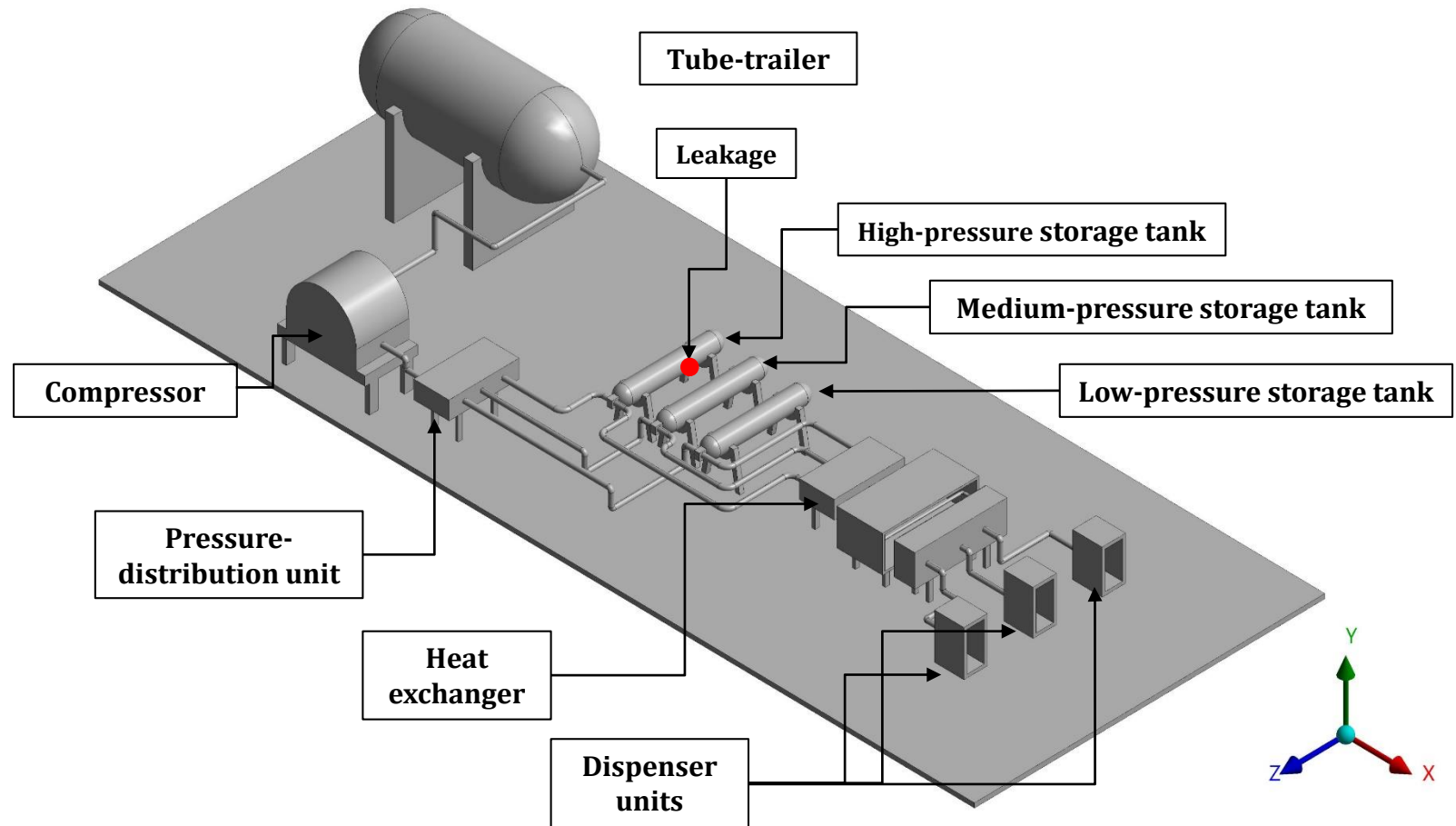
$$\frac{\partial \bar{\rho} \tilde{u}_i}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_i \tilde{u}_j}{\partial x_j} + \frac{\partial \bar{p}}{\partial x_i} - \frac{\partial \bar{\sigma}_{ij}}{\partial x_j} = -\frac{\partial \bar{\rho} \tau_{ij}^r}{\partial x_j} + \frac{\partial}{\partial x_j} (\bar{\sigma}_{ij} - \bar{\sigma}_{ij})$$

$$\frac{\partial E_f}{\partial t} + \bar{u}_j \frac{\partial E_f}{\partial x_j} + \frac{1}{\rho} \frac{\partial \bar{u}_i \bar{p}}{\partial x_i} + \frac{\partial \bar{u}_i \tau_{ij}^r}{\partial x_j} - 2\nu \frac{\partial \bar{u}_i \bar{S}_{ij}}{\partial x_j} = -\epsilon_f - \pi$$

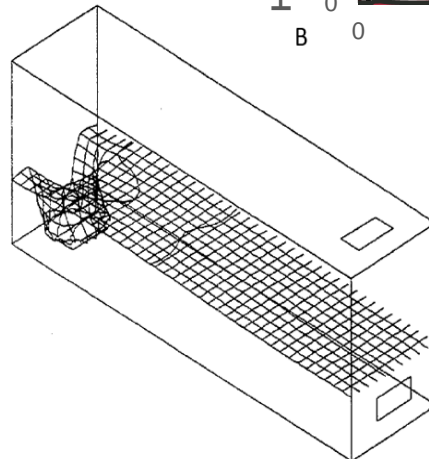
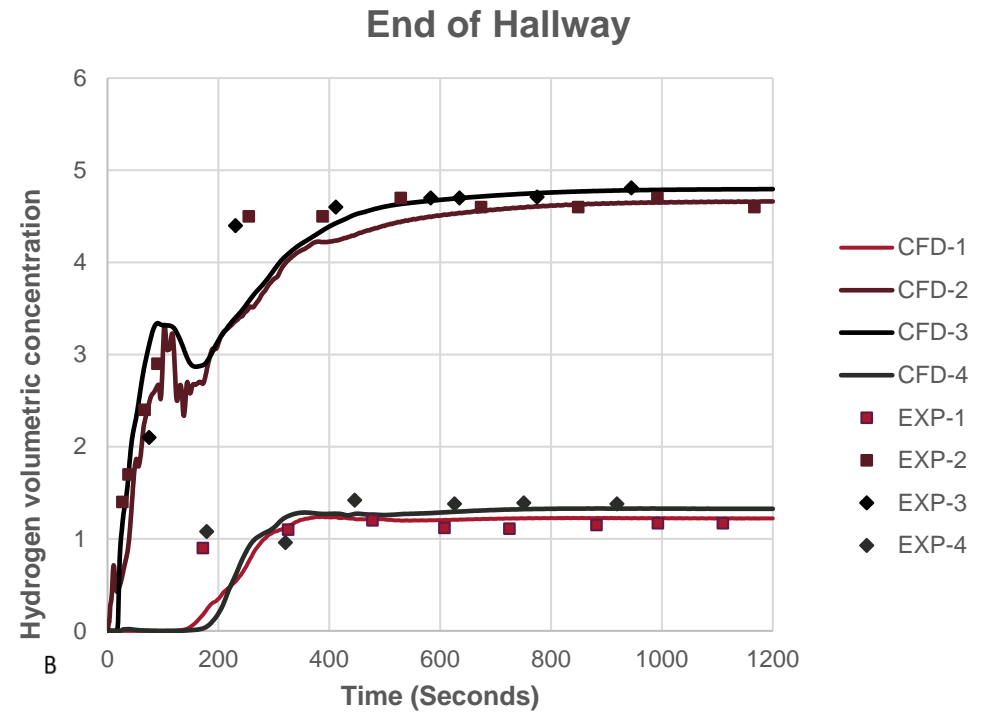
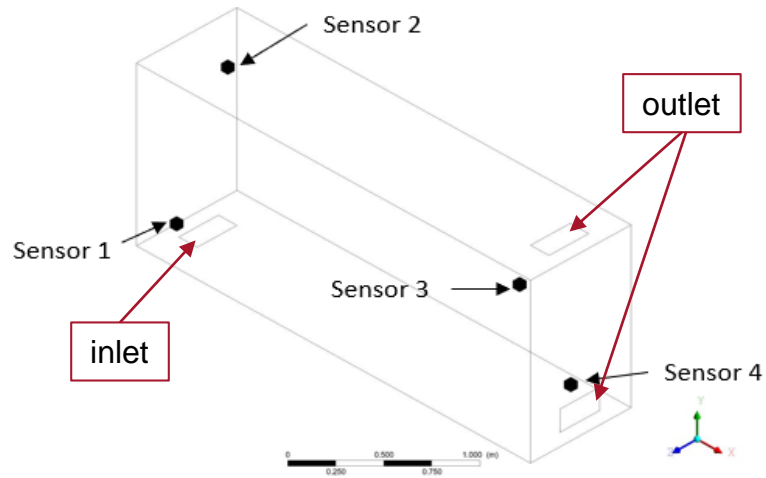
$$\frac{\partial \bar{\rho} \bar{Y}_\alpha}{\partial t} + \frac{\partial \bar{\rho} \tilde{u}_j \bar{Y}_\alpha}{\partial x_j} = \frac{\partial}{\partial x_j} \left(\bar{\rho} (\tilde{u}_j \bar{Y}_\alpha - \bar{u}_j \bar{Y}_\alpha) - \bar{\rho} \bar{D}_\alpha \frac{\partial \bar{Y}_\alpha}{\partial x_j} \right) + \bar{\omega}_\alpha$$



Hydrogen refuelling station



Hydrogen dispersion



Hydrogen concentration of 1%

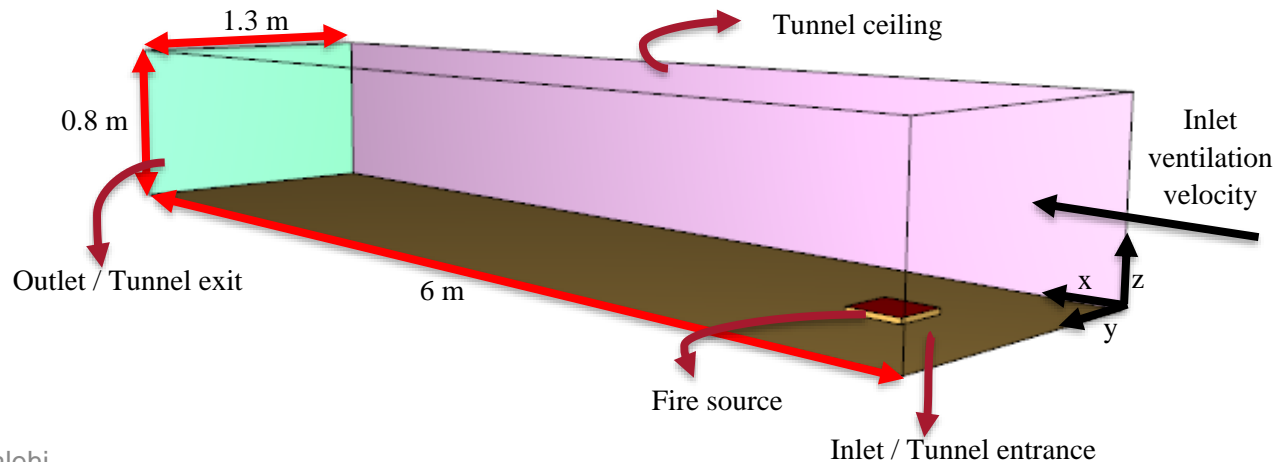
Hydrogen fire



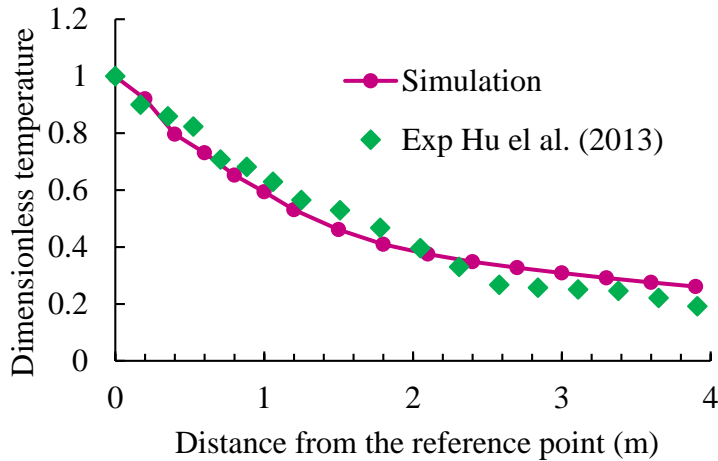
(Fuel Leak Simulation. Swan et al., 2001)

Simulation set	Inlet ventilation velocity (m/s)	Fuel type	Slope (%)	Storage capacity (%)
I	0, 1.2	Hydrogen	0	100
	0, 1.2	Propane		
II	0, 0.6, 1.2	Hydrogen	0, 3, 6, 9	100

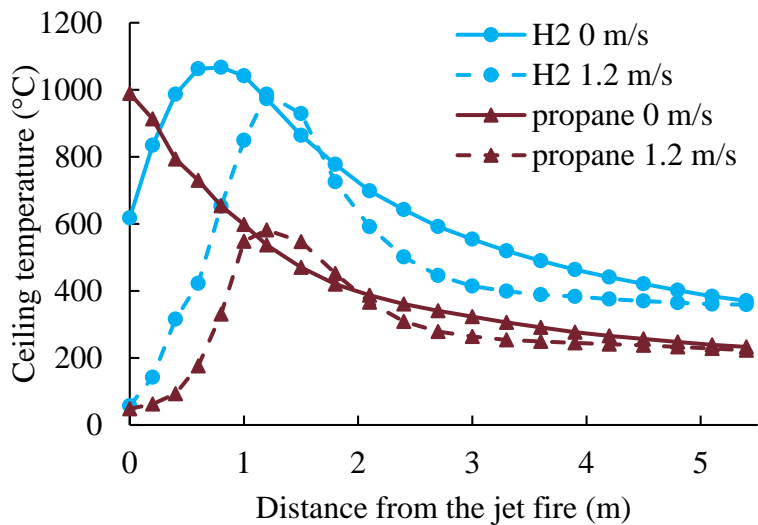
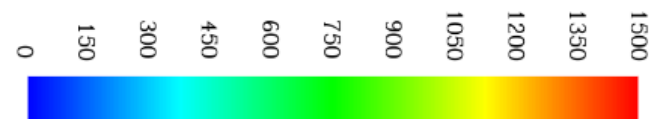
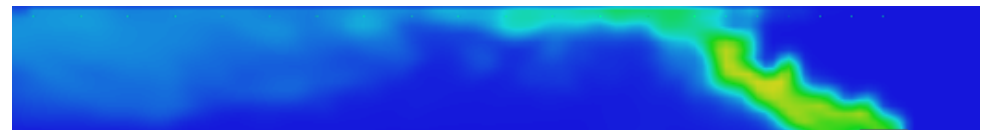
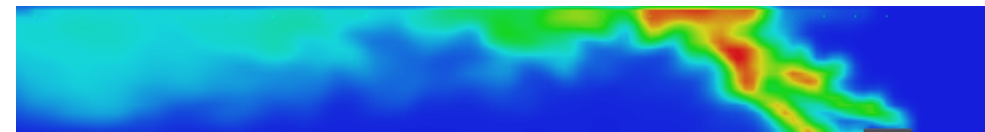
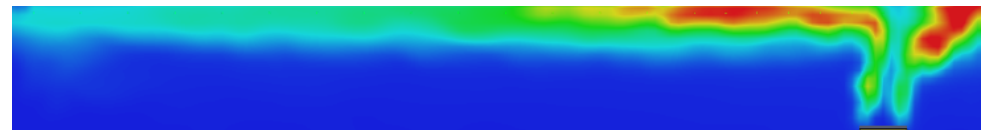
Fuel type	Burner Size	HRRPUA	ΔH_c	HRR
Hydrogen	0.09 m ²	8,900 kW/m ²	119.7 MJ/kg	801 kW
Propane		4,564 kW/m ²	45.8 MJ/kg	410 kW



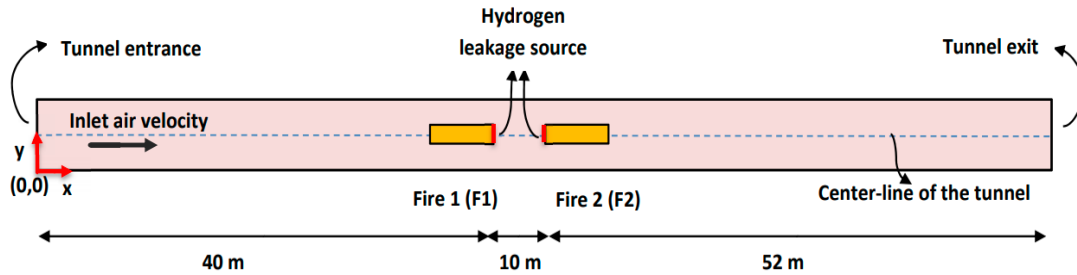
Hydrogen versus propane fire



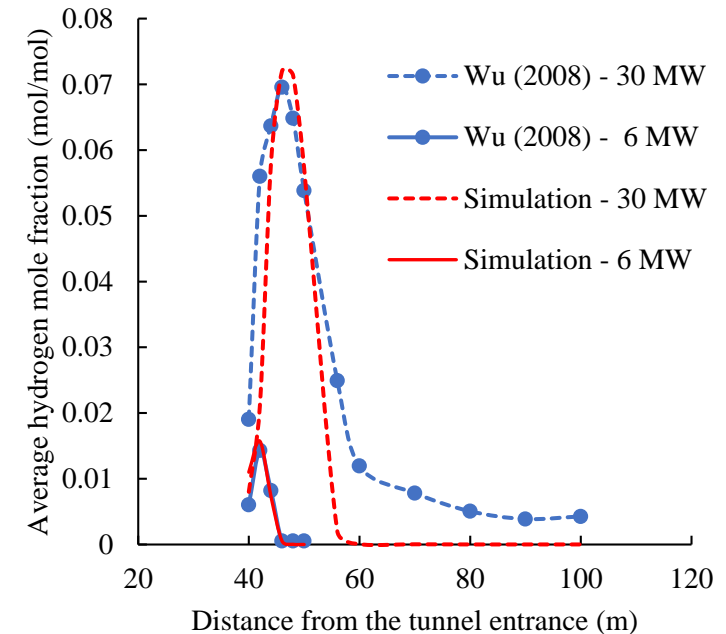
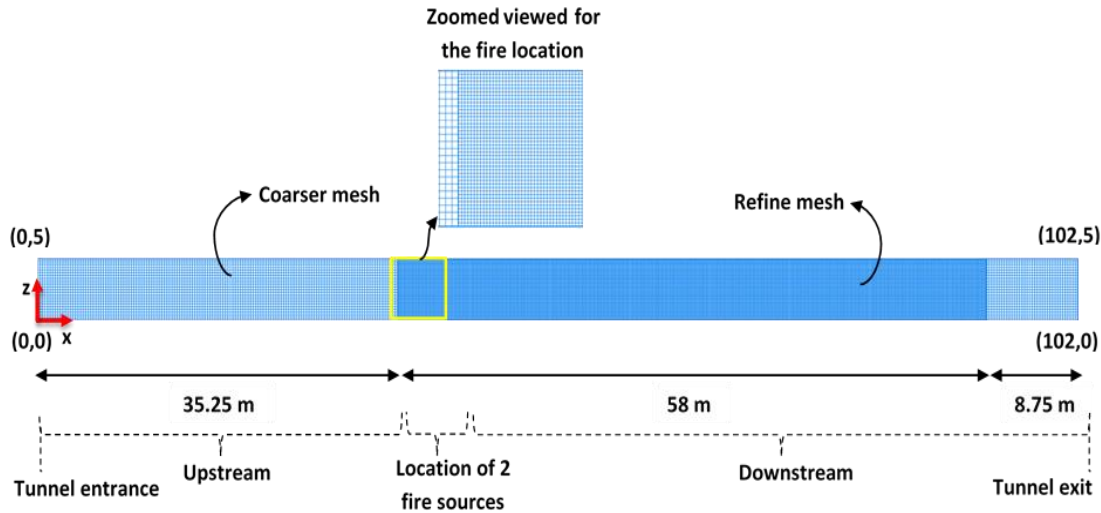
$$\frac{\Delta T_x}{\Delta T_0} = \frac{T_x - T_a}{T_0 - T_a}$$



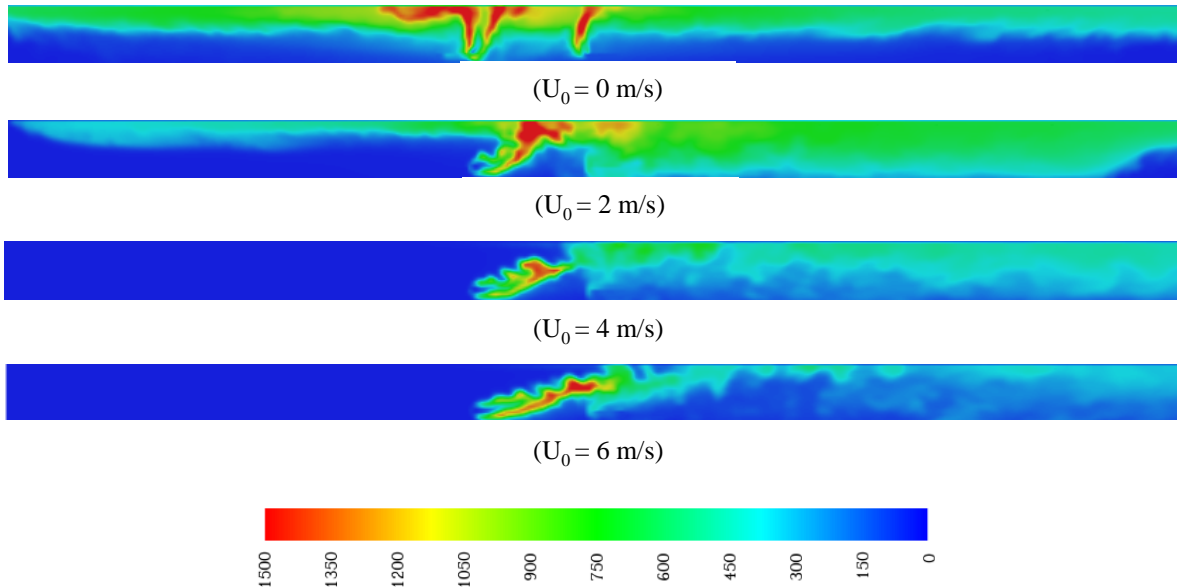
Multiple hydrogen fire



F1 (MW)	HRR	F2 (MW)	HRR	Slope (%)	Velocity (m/s)
5		40		0-5	0-7



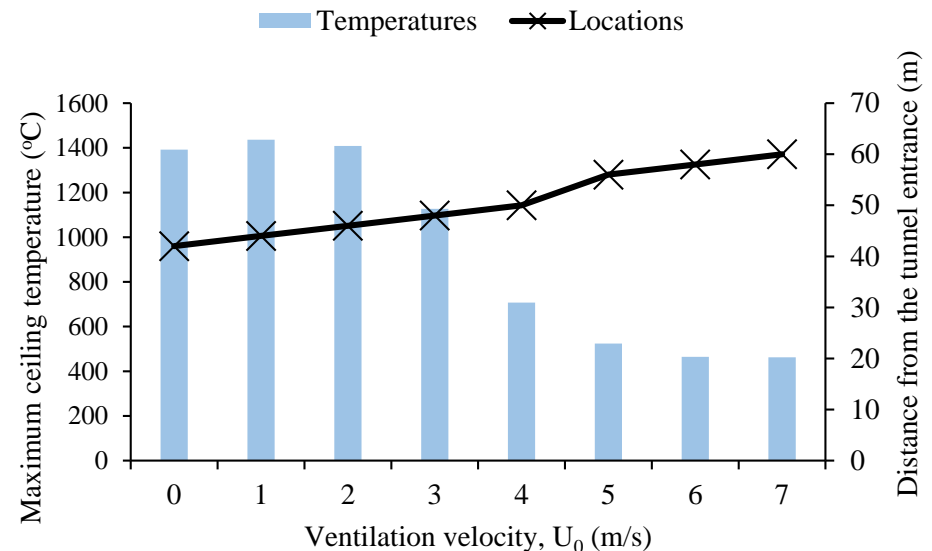
Multiple hydrogen fire



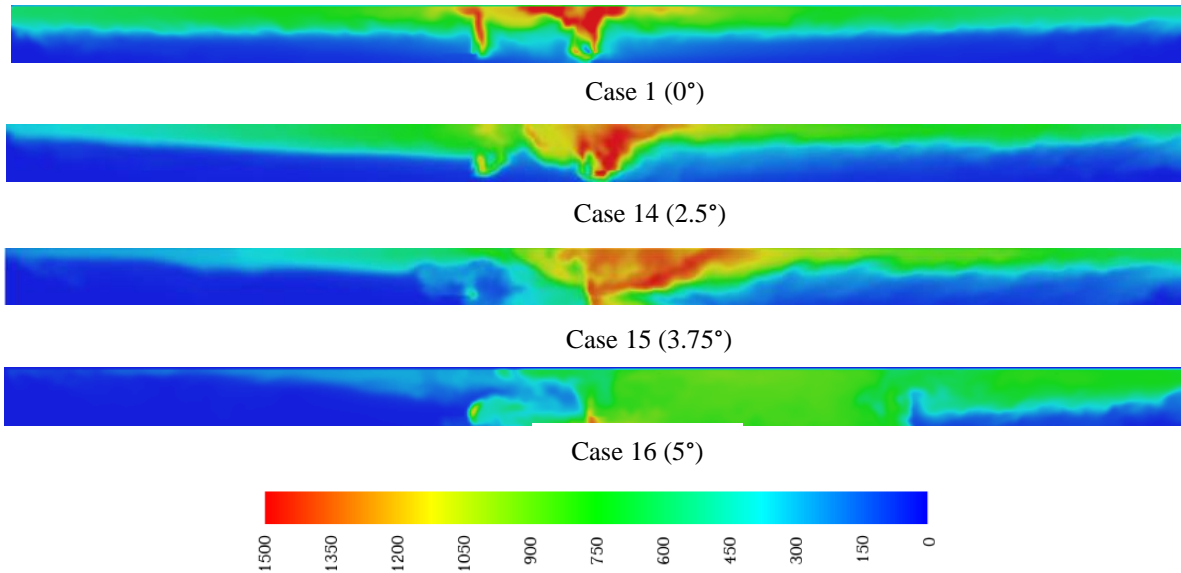
Ventilation velocity

- Air quality in the tunnel.
- Impacts of heat and smoke
- The egress of tunnel users
- Support firefighting

- Enhance the dispersion rate of hydrogen away from the combustion zone:
lowering of the combustion rate
- Better mixing of the hot vaporized fuel particles and oxygen:
enhance combustion rate



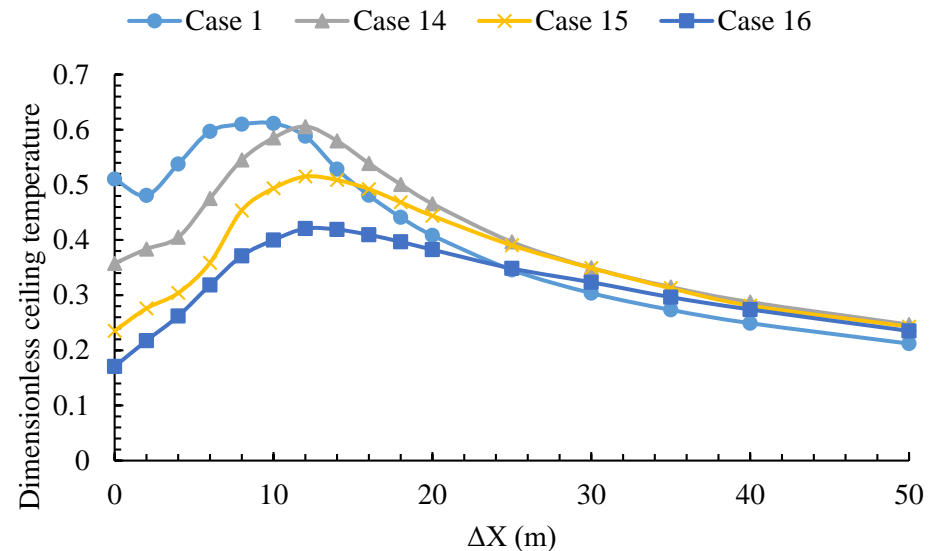
Multiple hydrogen fire



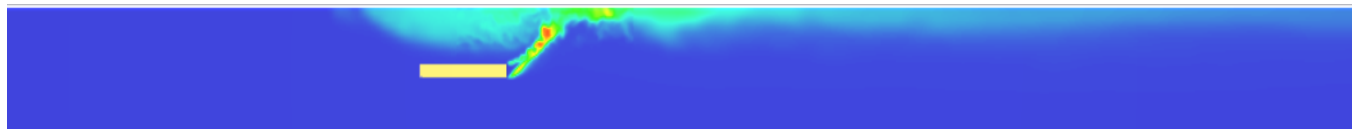
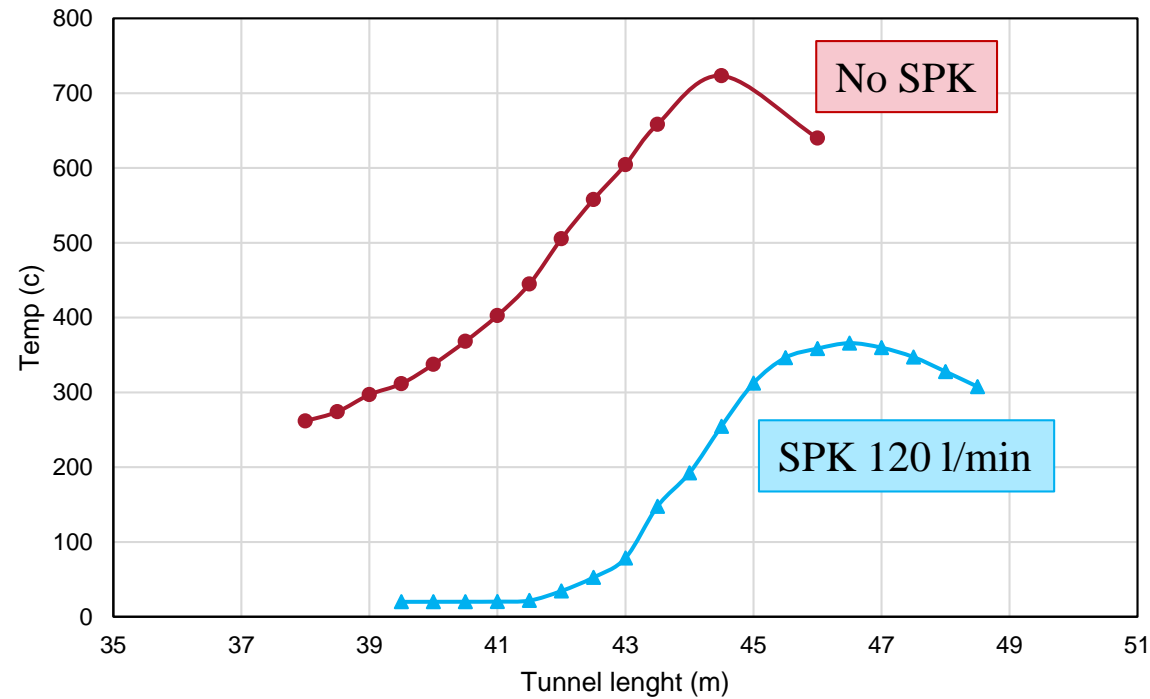
Tunnel slope

- 50 km/h: slope < 5%
- 30 km/h: slope < 8-9%

- Increasing the slopping clears the upstream from the hot gas, while spreading and covering them downstream
- The tilting of the flames in the direction of the slope: the shift of the peak ceiling temperature
- The rapid dispersion of the leaked hydrogen reduced the ceiling temperatures



Sprinkler - hydrogen fire



Thank you for your attention.

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